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On the Generation of Side-Edge Flap Noise

M. S. Howe

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On the Generation of Side-Edge Flap Noise

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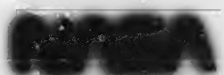

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TABLE OF CONTENTS

SUMMARY 1

1. INTRODUCTION 1

2. FORMULATION OF THE AERODYNAMIC SOUND PROBLEM IN TERMS OF DIFFRACTION THEORY 3

3. THE RADIATED SOUND 9

4. APPROXIMATE EVALUATION OF THE WAVENUMBER INTEGRALS 14

5. THE INTERRELATION BETWEEN THE SURFACE PRESSURE SPECTRUM AND THE ACOUSTIC SPECTRUM 16

6. COMPARISON WITH EXPERIMENT 25

7. CONCLUSIONS 27

APPENDIX A. THE GREEN'S FUNCTION FOR A NONCOMPACT SLOT 29

APPENDIX B. THE GREEN'S FUNCTION FOR A COMPACT SLOT 34

REFERENCES 40

LIST OF FIGURES

Figure 1. (a) The "clean" trailing edge is represented analytically by means of a semi-infinite rigid plate in a mean flow at speed U. (b) The side-edge gap formed when a part-span flap of chord L is deployed is modeled by a rectangular slot whose width 2s is equal to the mean width of a side-edge gap. (c) View of the slotted half-plane from downstream. 4

2. Illustrating the variation of the function $m(\lambda)$ defined in Appendix B and used in the definition of the compact Green's function, for $2s/L = 0.02, 0.05, 0.1$.... 13

3. Variation of $\Delta(\Omega)$ (equation (39)) with Strouhal number $\Omega = \omega L/U$ in the flyover plane $\phi = 0$, and for $M = 0.1$, $U_3/U = 0.2$, $2s/L = 0.1$ 18

4. As for Fig. 3 with $M = 0.3$ 19

5. As for Fig. 3 with $M = 0.5$ 20

6. The field shape $\Delta(\Omega)$ (equation (39)) in the flyover plane $\phi = 0$, for $\Omega = 0.4$, 4, 40 and for $M = 0.1$, $U_3/U = 0.2$, $2s/L = 0.1$ 22

7. As for Fig. 6 with $M = 0.3$ 23

8. As for Fig. 6 with $M = 0.5$ 24

SUMMARY

A theory is proposed for estimating the noise generated at the side edges of part span trailing edge flaps in terms of pressure fluctuations measured just in-board of the side edge of the upper surface of the flap. Asymptotic formulae are developed in the opposite extremes of Lorentz contracted acoustic wavelength large/small compared with the chord of the flap. Interpolation between these limiting results enables the field shape and its dependence on subsonic forward flight speed to be predicted over the whole frequency range. It is shown that the mean width of the side edge gap between the flap and the undeflected portion of the airfoil has a significant influence on the intensity of the radiated sound. It is estimated that the noise generated at a single side edge of a full scale part span flap can exceed that produced along the whole of the trailing edge of the flap by 3 dB or more.

1. INTRODUCTION

A significant proportion of the noise generated by an aircraft on approach to landing is attributable to the deployment of high lift airframe components such as slats and flaps. Conventional jet-noise is of diminished importance in such circumstances because the engines are generally operated at reduced thrust. Fink and Schlinker [1], Ahtye, Miller and Meecham [2] and Kendall and Ahtye [3] have identified the side edges of part span trailing edge flaps as important sources of the airframe noise. In particular, the extrapolation to full scale of the experimental results of Kendall and Ahtye [3] leads to sound pressure levels which fall only a few dB below flight data reported by Healy [4]. Hardin [5] has pointed out that the relative intensity of side edge sources could be substantially greater for future aircraft using high bypass ratio engines, which may well operate in the landing configuration with the jet stream impinging directly onto the side edges of flaps.

It is well known (Ffowcs Williams and Hall [6]) that unsteady flow in the vicinity of an edge is an important source of aerodynamic sound. The generation of noise by turbulent flow over the trailing edge of an airfoil has been extensively discussed in the literature [7]. The studies cited above, however, suggest that for deployed part span flaps it is predominantly the characteristics of the unsteady flow in the vicinity of the *side* edges which determine the level and properties of the edge-generated sound. The unsteady

motion in the neighborhood of a side edge is related to the presence of a component of mean flow about the edge. This flow results in the formation of a conventional tip vortex due to forward motion of a lifting airfoil, and is from the lower (pressure) to the upper (suction) surfaces of the flap, a separation bubble being formed on the upper surface at the edge. The relatively large amplitude unsteady edge flow is associated with the instability of this separated flow.

An idealized two-dimensional theory of the side-edge noise mechanism has been discussed by Hardin [5], who considered a flow inhomogeneity in the form of a chordwise orientated line vortex. Potential flow theory was used to model the mean flow about the side edge. By means of a detailed study of possible trajectories of the vortex, Hardin argued that under a wide range of conditions likely to be encountered in practice, the noise generated during the motion of the vortex around the side edge could be significantly greater than that produced by an equal (spanwise) vortex convecting in a mean boundary flow past a trailing edge. Such an idealized analysis can only be expected to yield possible trends, and, apart from considerations regarding the characterization of the unsteady edge flow, takes no account of important effects arising from the proximity of the wing ahead of the flap and of the side edges of the adjacent trailing edge of the wing. The latter are analogous to the so-called *installation effects*, which play an important role in determining the jet-noise of an aircraft (see Ref. 8, 9).

In this report a theory is proposed which permits one to estimate the importance of proximity effects on the side-edge noise sources and, in addition, the influence of varying the forward flight speed of the aircraft. To do this the trailing edge of the wing is modeled by means of a thin, rigid half-plane in the "clean" configuration. When a part-span flap is deployed the gap between the side-edge of the flap and the undeflected portion of the neighboring trailing edge is represented by means of a narrow slot in the half-plane which is at right angles to the trailing edge. The length of this slot is equal to the chord of the flap, and the width is taken to be equal to the mean distance between the side edges of the flap and the adjacent undeflected wing (see Fig. 1). The spanwise edge flow resulting from the additional lift generated by the flap is depicted schematically in Fig. 1(c). In using this model to calculate the radiated sound, the finite angle of deflection of the flap is neglected, except insofar as it determines the magnitude of the mean flow velocity about the side edge. This approximation should be adequate for moderate angles of deflection, say of the order of 10°, in

which case the spanwise component of the mean velocity on the upper surface close to the side edge is typically of order 0.2-0.3U, U being the forward flight speed [*10*].

The analytical problem of calculating the sound generated by turbulent fluctuations in the spanwise flow near the side edge is formulated in §2 in terms of the evanescent wave theory of Chandiramani [11] and Chase [*12,13*]. This involves the use of the aeroacoustic Green's function whose normal derivative vanishes on the slotted half-plane. Approximate representations of this Green's function in the opposite extremes in which the chord of the flap is large/small relative to the Lorentz contracted acoustic wavelength are obtained in Appendices A and B. These are used in §3 to determine the spectrum of the acoustic radiation in terms of the wavenumber-frequency spectrum of the surface pressure fluctuations just in-board of the side edge of the flap. The introduction of further simplifying assumptions (§§4,5) enables the acoustic spectrum to be expressed directly in terms of a surface pressure point frequency spectrum. Interpolation between the low and high frequency limits in this case yields the approximate dependence of the radiation on all relevant Strouhal numbers (based on the chord of the flap) and forward flight Mach numbers. In §6 a comparison is made with recent experimental results, and it is predicted that the noise generated at the side edge of a part span flap at full scale can exceed that generated along the whole of the trailing edge of the flap by up to 3 dB.

2. FORMULATION OF THE AERODYNAMIC SOUND PROBLEM IN TERMS OF DIFFRACTION THEORY

A semi-infinite rigid plate which occupies the half-plane ($x_1<0$, $x_2=0$) of a rectangular coordinate system (x_1,x_2,x_3) is taken to model the trailing edge of the "clean" airfoil. The aerodynamic sound generated when a part-span flap is deployed will be calculated by introducing a rectangular slot of length L and width 2s, with $2s \ll L$, to represent the side edge gap between the flap and the undeflected trailing edge. The slot occupies the region $(-L<x_1<0, x_2=0, |x_3|<s)$ of the half-plane, as illustrated in Fig. 1(b). The present analysis will take no account of the finite angle of deployment of the flap, although its influence is implicitly included in that it determines the magnitude of the mean flow about the side edge and the associated turbulence levels. In addition, the possible existence of a spanwise slot ahead of the flap [indicated by the dashed lines in Figs. 1(a), 1(b)] is ignored, as is the small finite extension of the flap beyond the nominal

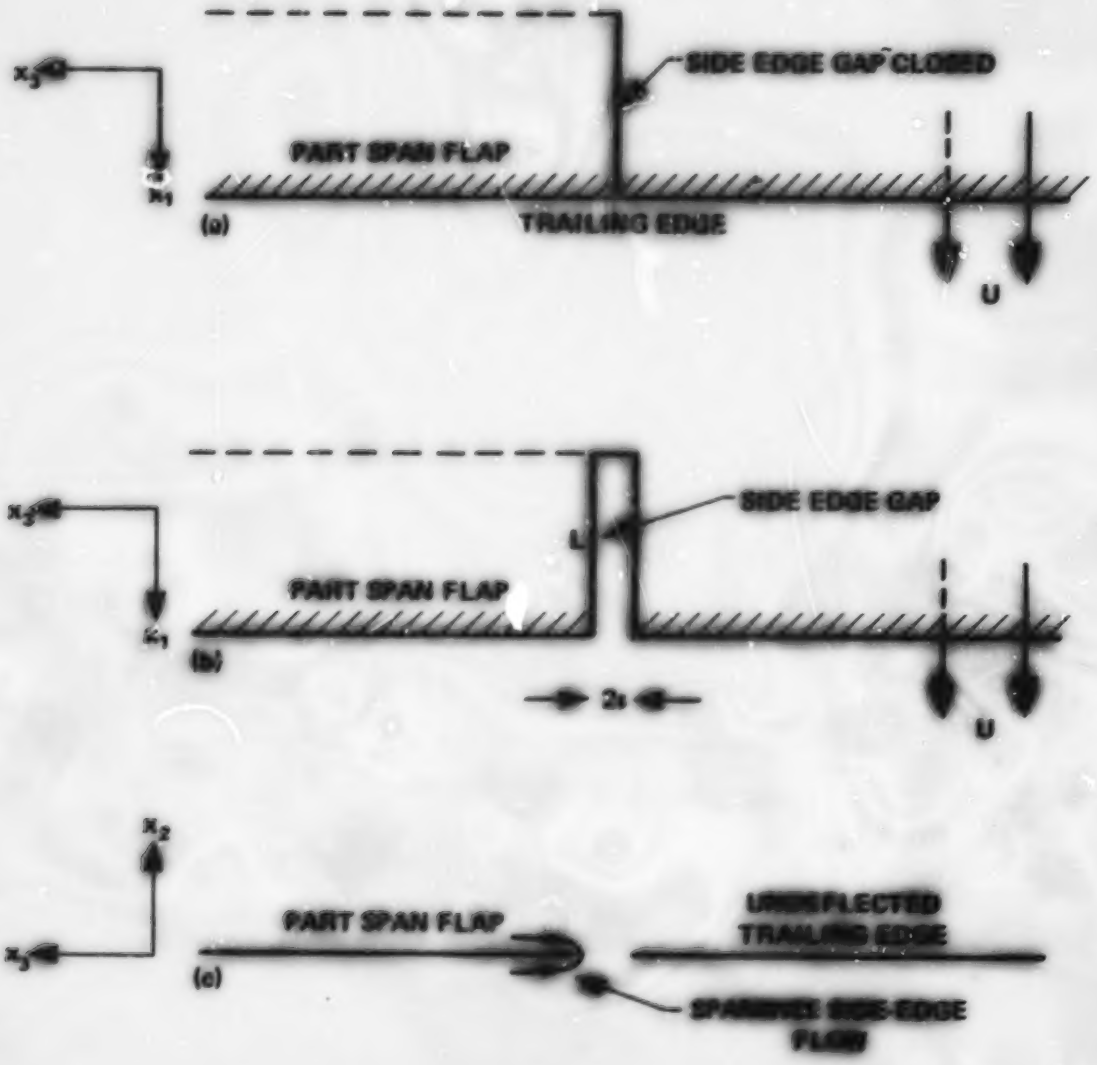

FIG. 1. (a) THE "CLEAN" TRAILING EDGE IS REPRESENTED ANALYTICALLY BY MEANS OF A SEMI-INFINITE RIGID PLATE IN A MEAN FLOW AT SPEED U. (b) THE SIDE-EDGE GAP FORMED WHEN A PART-SPAN FLAP OF CHORD L IS DEPLOYED IS MODELED BY A RECTANGULAR SLOT WHOSE WIDTH 2s IS EQUAL TO THE MEAN WIDTH OF A SIDE-EDGE GAP. (c) VIEW OF THE SLOTTED HALF-PLANE FROM DOWNSTREAM. IN CALCULATING THE NOISE THE FINITE ANGLE OF DEPLOYMENT OF THE FLAP IS NEGLECTED. THE FLAP OCCUPIES THE REGION $(-L<x_1<0, x_2=0, x_3>s)$.

trailing edge ($x_1=x_2=0$) of the wing. Forward flight is represented by a uniform mean flow on both sides of the airfoil at subsonic speed U in the positive direction of the x_1-axis.

The instability of the separated spanwise flow over the upper surface of the flap near the side edge gives rise to turbulent surface pressure fluctuations whose magnitudes in the immediate vicinity of the edge are influenced by the presence of the slot. It is convenient to characterize these surface pressures in terms of an hypothetical surface pressure $P(x_1,x_3,t)$ say, that the same turbulence would induce on a plane rigid wall lying in $x_2 = 0$. If it could be assumed that the turbulence convects in a frozen pattern over the flap, P would be equal to the surface pressure fluctuation at distances in-board from the edge which exceed the correlation scale of the turbulence. The formulation of the noise problem in terms of P is equivalent to the use of "evanescent wave theory" in the calculation of trailing edge noise [*11-13*]. The principal advantage in the use of P is that it may be assumed to possess local spatial stationarity in the spanwise direction, a property not shared by the actual surface pressure close to the side edge. In practice, surface pressure measurements in-board of the edge would have to be used to quantify turbulence decay, etc., and thereby to estimate an approximate form of P near the edge (c.f., the analogous measurements performed by Brooks and Hodgson [*14*]).

Consider an elementary turbulent boundary layer disturbance above the flap (in $x_2>0$) which is proportional to $\exp\{i(k_1x_1+k_3x_3-\omega t)\}$. Henceforth, we shall omit from our formulae explicit reference to the exponential time factor $e^{-i\omega t}$. Practically all of the turbulence energy will be associated with disturbances having subsonic phase velocities in the (x_1-x_3)-plane. Hence, if the flap and airfoil were absent, the corresponding perturbation pressure would decay exponentially with perpendicular distance below the boundary layer, and would form an *evanescent* wave whose pressure signature p_I could be expressed as

$$p_I = \hat{p}_I(k_1,k_3,\omega)e^{i(k_1x_1+k_3x_3)+\Gamma x_2} \qquad (1)$$

where $\Gamma = \Gamma(k_1,k_3,\omega)>0$. The functional form of Γ will be discussed below.

Just above the flap, at distances from the side and trailing edges which exceed $\sim 1/(k_1^2+k_3^2)^{\frac{1}{2}}$, the harmonic disturbance (1) gives rise to a specularly reflected pressure field such that the net surface pressure $P(x_1,x_2,t)$ is given by

$$P = \hat{P}(k_1,k_3,\omega)e^{i(k_1x_1+k_3x_3)} , \tag{2}$$

where,

$$\hat{P} = 2\hat{p}_I . \tag{3}$$

Sound waves are generated when the evanescent wave (1) is diffracted by inhomogeneities such as the edges of the flap. The side-edge flap noise corresponds to the diffraction radiation produced at the slot, and use of Eq. (3) in the diffraction calculation enables the acoustic pressure to be related directly to the surface pressure on the flap in-board of the side edge.

The diffraction problem is formulated as follows. Let p_S denote the diffracted component of the perturbation pressure. The net pressure is accordingly given by

$$p = p_I + p_S , \tag{4}$$

and is such that on the upper surface of the flap

$$p_S \to p_I , \; p \to P$$

at large distances from the slot and trailing edge. At large distances from the airfoil, p_S represents the acoustic radiation. In addition, p_S must be chosen to ensure that the normal velocity vanishes on the surface of the airfoil. In the high Reynolds number limit which is relevant in practice, unsteady viscous stresses may be neglected, and the x_2-component of the momentum equation implies that the normal component of velocity will vanish on the airfoil provided that

$$\partial p_I/\partial x_2 + \partial p_s/\partial x_2 = 0 \qquad (5)$$

on the upper and lower surfaces of the slotted half-plane.

Acoustic disturbances are convected by mean flow. Since, however, the nonuniform mean flow in the vicinity of the slot is localized, its effect on propagation will be neglected, and in the linearized approximation it therefore follows that p_s satisfies the time-harmonic convected wave equation:

$$\left\{\left(-ik_0 + M\frac{\partial}{\partial x_1}\right)^2 - \frac{\partial^2}{\partial x_j^2}\right\} p_s(\underline{x},\omega) = 0 \ , \qquad (6)$$

where $M = U/c < 1$ is the mean flow (flight) Mach number, $k_0 = \omega/c$ the acoustic wavenumber, and c is the speed of sound. The solution which satisfies the radiation condition of outgoing waves at large distances together with the surface condition (5) can be written down with the aid of a Green's function $G(\underline{x},\underline{y})$. This satisfies $\partial G/\partial x_2 = 0$ on the slotted half-plane, the radiation condition, and equation (6) when the right hand side is replaced by the point source $\delta(\underline{x}-\underline{y})$. According to the reverse-flow reciprocal theorem [*15*], $G(\underline{x},\underline{y})$ is also a solution as a function of $\underline{y}$ of the adjoint or ***reverse flow*** problem:

$$\left\{\left(-ik_0 - M\frac{\partial}{\partial y_1}\right)^2 - \frac{\partial^2}{\partial y_j^2}\right\} G(\underline{x},\underline{y}) = \delta(\underline{x}-\underline{y}) \ , \qquad (7)$$

and satisfies the radiation condition and $\partial G/\partial y_2 = 0$ on the slotted half-plane. In the reciprocal problem the source $\delta(\underline{x}-\underline{y})$ is situated at the ***observer*** position $\underline{x}$ and generates a disturbance which propagates in $\underline{y}$-space in a medium moving at speed U in the ***negative*** y_1-direction.

A formal representation of the radiated sound is obtained by means of Kirchhoff's integration procedure ([*16*], Chap. 8). In equation (6) replace the dummy variable $\underline{x}$ by $\underline{y}$, multiply by $G(\underline{x},\underline{y})$ and integrate with respect to $\underline{y}$ over the region of space bounded by the airfoil and a large sphere of radius R^*, say. Similarly, multiply Eq. (7) by $p_s(\underline{y})$ and integrate over the same region. Subtract the two results and apply the divergence theorem to obtain, as $R^* \to \infty$:

$$p_S(\underline{x},\omega) = \oint_{S_{\pm}} G(\underline{x},\underline{y}) \cdot \frac{\partial p_s}{\partial y_n}(\underline{y})dy_1 dy_3 \ , \qquad (8)$$

where the integration is over the upper and lower surfaces $S_{\pm}$ respectively of the slotted half-plane, and y_n is in the direction of the outward normal. In obtaining this expression the radiation condition has been used to eliminate contributions from the surface of the sphere, and use has been made of $\partial G/\partial y_2 = 0$ on the rigid surface of the airfoil. Equation (8) is expressed in terms of the *incident*, evanescent wave p_I by means of equation (5), expressed in the form

$$\partial p_S/\partial y_n = \mp \partial p_I/\partial y_2 \qquad (9)$$

on $S_{\pm}$. If we next define

$$G_{\pm}(\underline{x}) = G(\underline{x},y_1,\pm 0,y_3) \ , \qquad (10)$$

equation (8) becomes:

$$p_S(\underline{x},\omega) = -\int_{S_+} [G_+(\underline{x})-G_-(\underline{x})] \frac{\partial p_I}{\partial y_2}(\underline{y})dy_1 dy_3 \ , \qquad (11)$$

the integration being over that portion of the *upper* surface of the slotted airfoil wherein $\partial p_I/\partial y_2$ is different from zero. Using equations (1), (3) and summing over all possible values of the wavenumbers k_1, k_3, the radiation is expressed, finally, in terms of the surface pressure amplitude coefficient $\hat{P}(k_1,k_3,\omega)$:

$$p_S(\underline{x},\omega) =$$

$$-\tfrac{1}{2}\int_{-\infty}^{\infty}\int dk_1 dk_3 \Gamma(k_1,k_3,\omega)\hat{P}(k_1,k_3,\omega)\int_{S_+} [G_+(\underline{x})-G_-(\underline{x})]e^{i(k_1 y_1+k_3 y_3)} dy_1 dy_3$$

. (12)

Equation (12) may be used to express the frequency spectrum $S(\underline{x},\omega)$, say, of the acoustic radiation in terms of the wavenumber-frequency spectrum $\Pi(k_1,k_3,\omega)$ of the surface pressure $P(x_1,x_3,t)$. We recall that these quantities are defined through the relations:

$$\langle p_s(\underline{x},t)p_s(\underline{x},t+\tau)\rangle = \int_{-\infty}^{\infty} S(\underline{x},\omega)e^{-i\omega\tau}d\omega \quad , \tag{13}$$

$$\langle P(y_1,y_3,t)P(y_1+\bar{y}_1,y_3+\bar{y}_3,t+\tau)\rangle$$

$$= \iiint_{-\infty}^{\infty} \Pi(k_1,k_3,\omega)e^{i(k_1\bar{y}_1+k_3\bar{y}_3-\omega\tau)}dk_1dk_3d\omega \quad , \tag{14}$$

in which the angle brackets denote an ensemble average. Introducing the hypothesis that $P(y_1,y_3,t)$ is locally a stationary random function of its arguments, with zero mean (a reasonable assumption inasmuch as P is defined independently of the diffracted field), it follows that:

$$\langle \hat{P}(k_1,k_3,\omega)\hat{P}(\bar{k}_1,\bar{k}_3,\bar{\omega})\rangle$$

$$= \delta(k_1+\bar{k}_1)\delta(k_3+\bar{k}_3)\delta(\omega+\bar{\omega})\Pi(k_1,k_3,\omega) \quad , \tag{15}$$

and similarly that:

$$\langle p_s(\underline{x},\omega)p_s(\underline{x},\bar{\omega})\rangle = \delta(\omega+\bar{\omega})S(\underline{x},\omega) \quad . \tag{16}$$

These results will be used below.

3. THE RADIATED SOUND

The practical implementation of the formal solution (12) requires a knowledge of the Green's function $G(\underline{x},\underline{y})$. Approximate analytical representations of G are available in the two asymptotic extremes in which the chord L of the flap satisfies

$$k_0L/(1-M^2) >> \ , \ << 1 \quad . \tag{17}$$

The details of the calculation of G in these two cases are outlined in the Appendices under the additional restriction that $k_0 s \ll 1$, i.e., that the acoustic wavelength is large compared with the side edge gap.

Attention will be confined to the side-edge noise problem in which $P(y_1,y_3,t)$ may be taken to be nonzero only in the immediate vicinity of the slot on the upper surface of the flap ($-L<y_1<0, y_2=+0, y_3>s$). The *noncompact* slot ($k_0 L>>1$) is discussed in Appendix A, and it follows from Eq. (A20) that, when the observer is in the far field, and $y_3>s$ (on the upper surface of the flap),

$$G_+(\underline{x})-G_-(\underline{x}) = \frac{F_{NC} e^{ik_0 r}}{r} \cdot \ln\left[\frac{y_3}{s} + \sqrt{\frac{y_3^2}{s^2} - 1}\right], \qquad (18)$$

where

$$F_{NC} = \frac{-i}{\pi^2(1+M\cos\theta)\{1 + \frac{2i}{\pi}\cdot\ln[\underline{C}k_0 s\cdot\sin\theta/4(1+M\cos\theta)]\}} \qquad (19)$$

and $\underline{C} = 1.78107...$ is the Euler-Mascheroni constant. In these expressions the observer position relative to the airfoil is specified in a form appropriate to aircraft flight at speed U in the negative x_1-direction by spherical polar coordinates (r,θ,ϕ) at the *time of emission of the received sound*, where the polar angle θ is measured from the positive direction of the x_1-axis [see Eqs. (A.18) of Appendix A]. The emission-time distance r is given by

$$r = \frac{1}{(1-M^2)^{\frac{1}{2}}}\left\{\frac{-M(x_1-y_1)}{(1-M^2)^{\frac{1}{2}}} + \sqrt{\frac{(x_1-y_1)^2}{1-M^2} + x_2^2 + x_3^2}\right\}. \qquad (20)$$

Substituting from (18) into Eq. (12), we find, as $k_0 r \to \infty$:

$$p_s(\underline{x},\omega) \simeq$$

$$\iint_{-\infty}^{\infty} dk_1 dk_3 \, \frac{r\hat{P}\hat{F}_{NC}}{2r_0} \int_{-L}^{0} e^{i(k_0 r + k_1 y_1)} dy_1 \int_{S}^{\infty} e^{ik_3 y_3} \ln\left[\frac{y_3}{s} + \sqrt{\frac{y_3^2}{s^2} - 1}\right] dy_3 \,, \quad (21)$$

in which the spanwise integration has been extended to $y_3 = +\infty$ since in practice the span of the flap will be large compared with the characteristic turbulence scale. Convergence of the integral in this limit is ensured by assigning to k_3 a small positive imaginary component which is subsequently allowed to vanish. The distance r_0 is defined by Eq. (20) when $y_1 = 0$, and to leading order we have:

$$r = r_0 - y_1 \cos\theta/(1+M)(1+M\cos\theta) \,, \quad (22)$$

where use has been made of the relations (A18). It follows from this and the integral definition of the Hankel function $H_0^{(1)}(z)$ ([17], page 955), that

$$p_s(\underline{x},\omega) \simeq \iint_{-\infty}^{\infty} \frac{\pi \hat{P}\hat{F}_{NC} H_0^{(1)}(k_3 s)}{2k_3 r_0} \cdot \frac{\sin\{\frac{1}{2}L[k_1 - k_0\cos\theta/(1+M)(1+M\cos\theta)]\}}{[k_1 - k_0\cos\theta/(1+M)(1+M\cos\theta)]}$$

$$\times \exp\{i[k_0 r_0 - \tfrac{1}{2}L(k_1 - k_0\cos\theta/(1+M)(1+M\cos\theta))]\} dk_1 dk_3 \,. \quad (23)$$

Let $S_{NC}(\omega)$ denote the frequency spectrum of the acoustic pressure in the noncompact limit, defined as in Eq. (16). Equation (23) can be used to form the product on the left of (16) which, used in conjunction with Eq. (15), yields:

$$S_{NC}(\omega) \simeq \frac{\pi^2 |F_{NC}|^2}{4r_0^2} \int\int_{-\infty}^{\infty} \left| \frac{\Gamma H_0^{(1)}(k_3 s)}{k_3} \right|^2 \Pi(k_1, k_3, \omega) \times$$

$$\times \frac{\sin^2\{\frac{1}{2}L[k_1 - k_0\cos\theta/(1+M)(1+M\cos\theta)]\}}{\{k_1 - k_0\cos\theta/(1+M)(1+M\cos\theta)\}^2} \, dk_1 dk_3 \, . \qquad (24)$$

The formulae given in Appendix B for the Green's function for a *compact slot* $[k_0 L/(1-M^2) \ll 1]$ may be used similarly to calculate the corresponding acoustic pressure spectrum $S_C(\omega)$, say. One finds in this case:

$$S_C(\omega) \simeq$$

$$\frac{\pi^2}{16}\left(\frac{L}{r_0}\right)^2 |F_C|^2 \int\int_{-\infty}^{\infty} \left| \frac{\Gamma f(k_1 L) H_0^{(1)}(k_3 s)}{k_3} \right|^2 \Pi(k_1, k_3, \omega) dk_1 dk_3 \, , \qquad (25)$$

in which

$$F_C = \left[\frac{2k_0 L\{(M+\cos\theta)^2 + (1-M^2)\cos^2\phi \sin^2\theta\}^{\frac{1}{2}}}{i\pi(1-M^2)(1+M\cos\theta)} \right]^{\frac{1}{2}} \frac{\sin(\frac{1}{2}\bar{\theta})}{\pi(1+M\cos\theta)} \, , \qquad (26)$$

$$f(z) = \int_0^1 m(\lambda) e^{-iz\lambda} d\lambda \, . \qquad (27)$$

The function $m(\lambda)(0<\lambda<1)$ is defined in Appendix B, and depends on the value of the slot width/length ratio $2s/L$. Its behavior for $2s/L = 0.02, 0.05, 0.1$ is illustrated in Fig. 2. The angle $\bar{\theta}$ is given in terms of (θ, ϕ) by Eq. (B19). When $\phi = 0$, i.e., in the "flyover" plane, we have

$$\sin(\tfrac{1}{2}\bar{\theta}) = \sin(\tfrac{1}{2}\theta)\{(1-M)/(1+M\cos\theta)\}^{\frac{1}{2}} \, . \qquad (28)$$

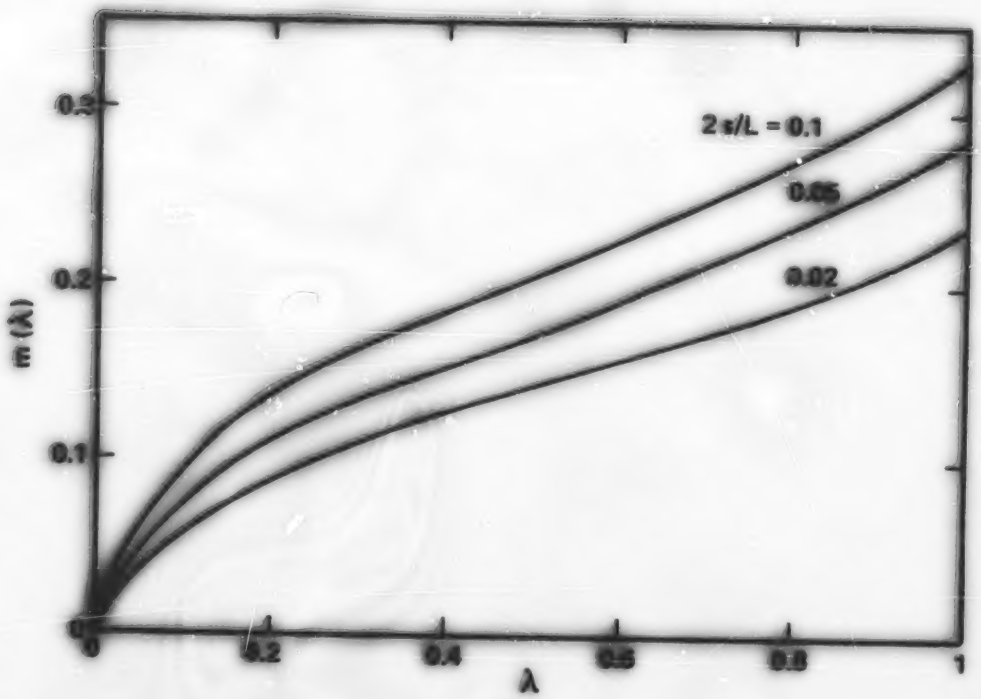

FIG. 2. ILLUSTRATING THE VARIATION OF THE FUNCTION $m(\lambda)$ DEFINED IN APPENDIX B AND USED IN THE DEFINITION OF THE COMPACT GREEN'S FUNCTION, FOR $2s/L = 0.02, 0.05, 0.1$.

It should be noted that Eqs. (24), (25) specify the acoustic spectrum in terms of the frequency ω as measured by an observer fixed relative to the airfoil. This is related to the frequency ω' that would be measured by an observer at rest relative to the mean flow by the usual Doppler relation $\omega' = \omega/(1+M\cos\theta)$.

4. APPROXIMATE EVALUATION OF THE WAVENUMBER INTEGRALS

The integrals in Eqs. (24), (25) can be estimated by first noting that, in the region in which the surface pressure spectrum $\Pi(k_1,k_3,\omega)$ is significantly different from zero, $k_1L \gg 1$ (i.e., turbulence scales are small compared with the chord of the flap), and therefore that the sine in Eq. (24) and $f(k_1L)$ in (25) will vary rapidly with k_1. In the case of Eq. (24), this implies that the principal contribution to the k_1-integral is from the neighborhood of

$$k_1^* = k_0\cos\theta/(1+M)(1+M\cos\theta) \ . \tag{29}$$

At this relatively small value of k_1 the surface pressure spectrum is likely to be sharply peaked near $k_3 = \omega/U_3$, where U_3 is a velocity which is of the same order as the mean spanwise velocity component near the side edge. The value of the k_3-integral in (24) may accordingly be approximated by setting $k_3 = \omega/U_3$ in the integrand except in the argument of Π. Our approximate representation of $S_{NC}(\omega)$ is therefore:

$$S_{NC}(\omega) \simeq \frac{\pi^3 L}{8r_0^2} |F_{NC}|^2 \left| \frac{\Gamma(k_1^*,\omega/U_3,\omega)H_0^{(1)}(\omega s/U_3)}{\omega/U_3} \right|^2$$

$$\times \int_{-\infty}^{\infty} \Pi(k_1^*,k_3,\omega)dk_3 \ . \tag{30}$$

Further reduction of this result is achieved by observing that, if it can be assumed that the evanescent wave (1) is convected by the mean flow in the same way as acoustic waves, we have

$$\Gamma = \{k_1^2+k_3^2-(k_0-Mk_1)^2\}^{\frac{1}{2}} \ . \tag{31}$$

But $M_3 = U_3/c \sim 0.2M$ (see Ref. 10) for moderate subsonic mean flow Mach numbers M. It follows that M_3^2 is generally negligible compared with unity, and when this is used in (31) with $k_1 = k_1^*$, it can be seen that in (30) we may take

$$\Gamma = |k_3| = |\omega|/U_3 \ . \tag{32}$$

It may be remarked that this approximation indicates that the possible uncertainty in the precise value of the convection velocity to be used in the definition of Γ is unlikely to be significant.

Similarly, k_1^* may be replaced by zero in the integrand of Eq. (30), since for small spanwise Mach number M_3 the acoustic wavelength will greatly exceed the characteristic turbulence scale. This approximation permits the introduction of the *point surface spectrum* $\Phi(\omega)$, defined by

$$\ell_1 \Phi(\omega) = \int_{-\infty}^{\infty} \Pi(0, k_3, \omega) dk_3 \ , \tag{33}$$

where $\ell_1 \sim U_3/\omega$ is the characteristic turbulence integral scale in the mean flow direction. This defines the local mean square surface pressure $P(x_1, x_3, t)$ through:

$$\langle P^2 \rangle = \int_{-\infty}^{\infty} \Phi(\omega) d\omega \ . \tag{34}$$

The use of Eq. (32), (33) in Eq. (30) gives our final approximation for the acoustic spectrum in the noncompact limit:

$$S_{NC}(\omega) \simeq \frac{\pi^3}{8} \left(\frac{\ell_1 L}{r_0^2} \right) |F_{NC}|^2 |H_0^{(1)}(\omega s/U_3)|^2 \Phi(\omega) \ . \tag{35}$$

Introducing the same approximations into the evaluation of the wavenumber integrals in Eq. (25), one obtains in the compact limit:

$$S_C(\omega) \simeq \frac{\pi^3}{8}\left(\frac{\ell_1 L}{r_0^2}\right)|F_C|^2|H_0^{(1)}(\omega s/U_3)|^2 I(2s/L)\Phi(\omega) , \qquad (36)$$

in which

$$I = \int_0^1 |m(\lambda)|^2 d\lambda . \qquad (37)$$

This integral is a function of the slot width/length ratio 2s/L, and typical values are given in Table 1:

TABLE 1

2s/L	0.02	0.05	0.1
I	0.022	0.033	0.046

5. THE INTERRELATION BETWEEN THE SURFACE PRESSURE SPECTRUM AND THE ACOUSTIC SPECTRUM

Equations (35), (36) provide an approximate relation between the acoustic frequency spectrum $S(\omega)$ and the point surface pressure spectrum $\Phi(\omega)$, although in practice $\Phi(\omega)$ should perhaps be regarded as a chordwise averaged spectrum. The chordwise correlation scale ℓ_1 is of order U_3/ω. To exhibit an explicit relationship between $S(\omega)$ and $\Phi(\omega)$ we shall write

$$\ell_1 = \alpha U/\omega , \qquad (38)$$

in which α is taken to be constant in the region in which $\Phi(\omega)$ is significantly different from zero. In order of magnitude it might be anticipated that $\alpha \sim U_3/U$, although its precise value will not be required in this section.

The quantity

$$\Delta(\omega) = 10.\log_{10}\{S(\omega)/\alpha\Phi(\omega)(L/r_0)^2\} , \qquad (39)$$

gives the relation in dB between the sound pressure level at frequency ω and the surface pressure spectrum. We now proceed to discuss the dependence of $\Delta(\omega)$ on the chordwise Strouhal number $\Omega = \omega L/U$ for radiation directions which lie in the *flyover plane* $\phi = 0$.

From Eq. (35) it is seen that the noncompact component $\Delta_{NC}(\Omega)$ is given by

$$\Delta_{NC}(\Omega) = 10\cdot\log_{10}\left\{\frac{|H_0^{(1)}[\Omega(U/U_3)(s/L)]|^2}{8\pi\Omega(1+M\cos\theta)^2\{1+(4/\pi^2)\ln^2[\underline{C}\Omega M(s/L)\sin\theta/4(1+M\cos\theta)]\}}\right\} \tag{40}$$

The noncompact approximation requires for its validity that $\omega L/c \gg 1$, $\omega s/c \ll 1$, so that the outer limits of validity of Eq. (40) are delimited by

$$1/M < \Omega < (L/s)/M \quad . \tag{41}$$

The corresponding compact component $\Delta_C(\Omega)$ is applicable for

$$\Omega \ll 1/M \quad , \tag{42}$$

and use of Eq. (28) in the flyover plane gives:

$$\Delta_C(\Omega) = 10\cdot\log_{10}\left\{\frac{M\sin^2(\tfrac{1}{2}\theta)I(2s/L)}{4(1+M)(1+M\cos\theta)^3}\,|H_0^{(1)}[\Omega(U/U_3)(s/L)]|^2\right\}. \tag{43}$$

Figures 3, 4, 5 illustrate the predicted variations in Δ_C (dashed curves) and Δ_{NC} (dotted) with Strouhal number Ω for three different radiation directions θ, and for forward flight Mach numbers $M = 0.1, 0.3, 0.5$ respectively. The slot width/length ratio $2s/L = 0.1$ and U_3/U is taken to be 0.2.

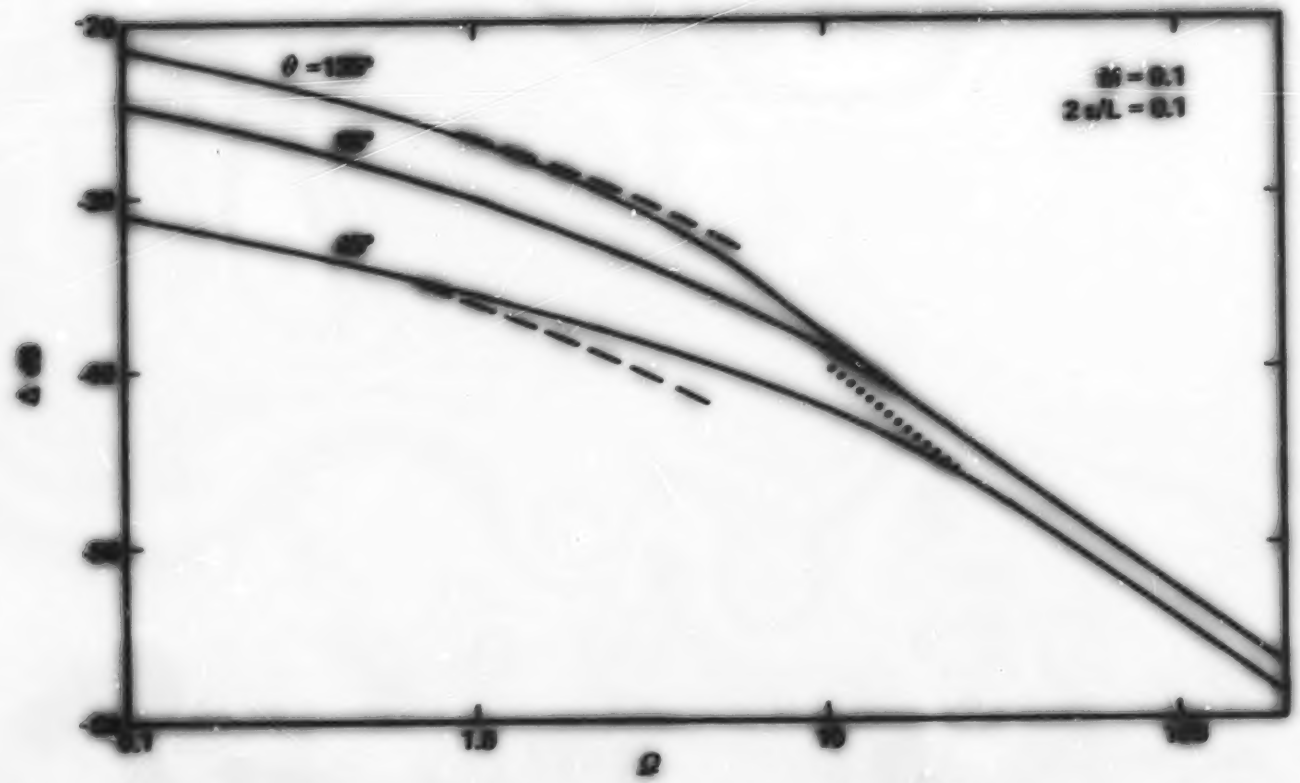

FIG. 3. VARIATION OF $\Delta(\Omega)$ (EQUATION (39)) WITH STROUHAL NUMBER $\Omega = \omega L/U$ IN THE FLYOVER PLANE $\phi = 0$, AND FOR $M = 0.1$, $U_3/U = 0.2$, $2s/L = 0.1$:
.... NONCOMPACT LIMIT OF EQUATION (40); ---- COMPACT LIMIT, EQUATION (39);
——— POSSIBLE INTERPOLATION CURVE. THE RADIATION ANGLE θ IS MEASURED FROM THE DOWNSTREAM DIRECTION.

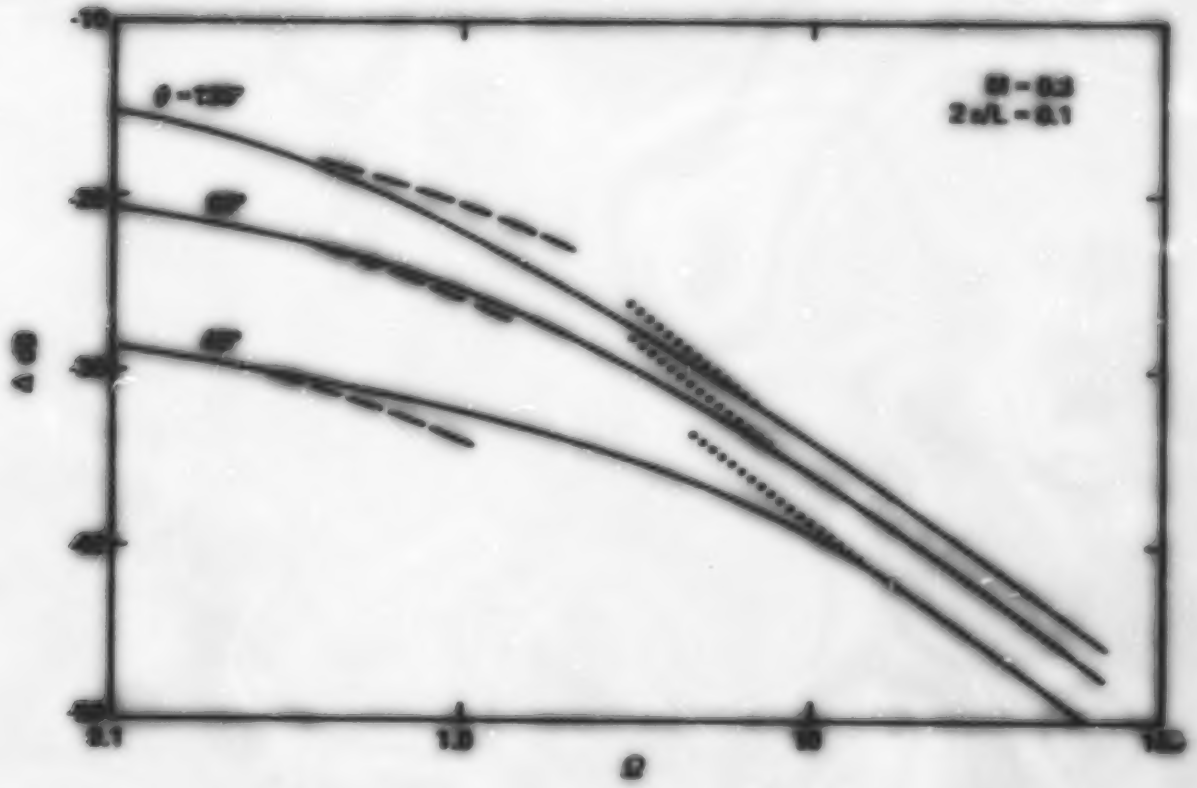

FIG. 4. AS FOR FIG. 3 WITH M = 0.3.

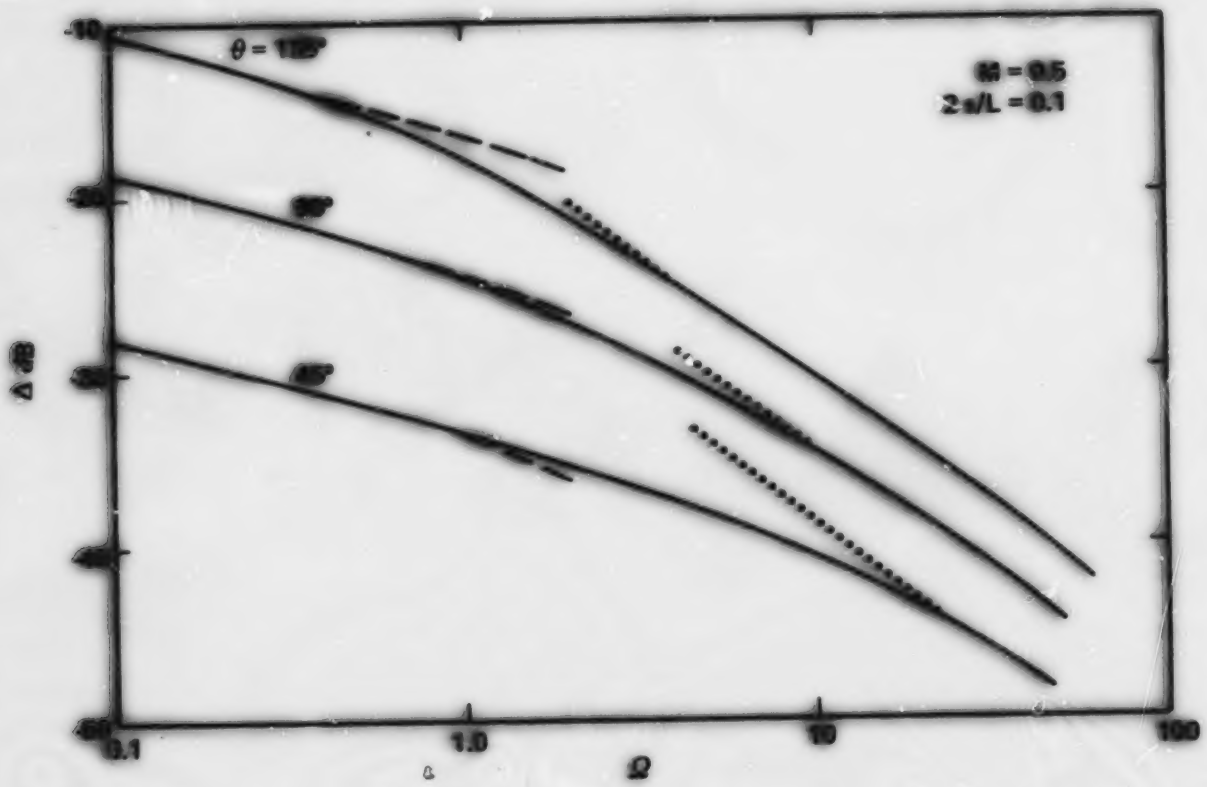

FIG. 5. AS FOR FIG. 3 WITH M = 0.5.

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The solid curves represent possible interpolative matchings between corresponding asymptotic approximations. There is a degree of arbitrariness in the choice of the interpolation curves, although it is unlikely that the errors involved will exceed about $\pm$ 3 dB. The divergence of these curves in each figure with decreasing Strouhal number indicates an accompanying change in effective acoustic source type. At high frequencies the radiation has monopole characteristics, modified by forward flight, and is associated with the unsteady flux through the slot induced by the side-edge turbulence. At low Strouhal numbers, however, that flux is equivalent to a dipole source at the edge of a semi-infinite rigid baffle, and the field shape peaks in the forward arc ($\theta = 180°$) with a null in the downstream direction.

The change in source type with Strouhal number can be illustrated further by means of the field shape plots of Figs. 6, 7, 8, which depict the variation of $\Delta(\Omega)$ with the flyover angle θ for $\Omega = 0.4, 4, 40$, and for the values of M, U_∞/U and $2s/L$ used above. The asymptotic formulae for Δ_C, Δ_{NC} have been used to draw the curves for $\Omega = 0.4, 40$. The data points at the intermediate Strouhal number $\Omega = 4$ have been obtained by making use of interpolation curves of the type shown in Figs. 3-5, and the corresponding field shape (dashed curves in Figs. 6-8) must therefore be regarded as tentative. The plots exhibit the forward flight amplification of sound radiated ahead of the aircraft ($\theta > 90°$), although its magnitude is dependent on the Strouhal number Ω. It is particularly noteworthy that, for nominally equal surface pressure fluctuations $\Phi(\omega)$, the semi-baffled dipole radiation at low Strouhal numbers is typically 10-25 dB greater than that from the higher frequency monopole sources. This is in contrast to the commonly accepted notions regarding the rank ordering of source strength with aeroacoustic source type. The difference arises because the effective monopole/dipole strength is proportional to the Hankel function $H_0^{(1)}(\omega s/U_\infty)$, which is small at high Strouhal numbers, but logarithmically large as $\Omega \to 0$. This influence of the finite mean width of the side-edge gap is a proximity effect, similar to the so-called installation effects which are known to be important in determining the jet noise of an aircraft [8,9]. Its occurrence in the present investigation emphasizes the importance of taking account of the neighboring undeflected portion of the trailing edge of the airfoil in estimating the radiated sound pressure level.

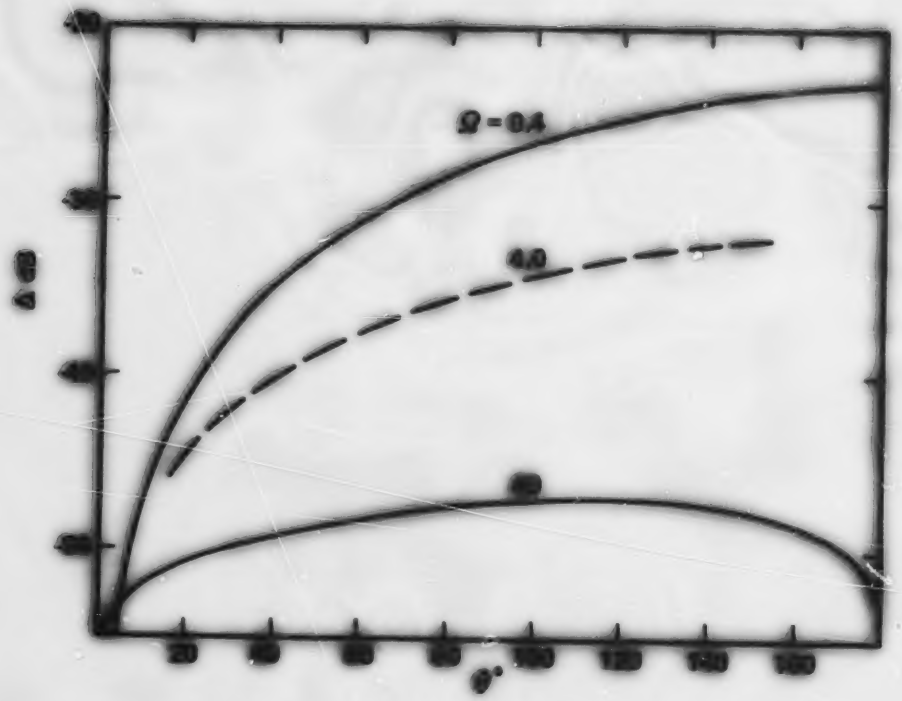

FIG. 6. THE FIELD SHAPE $\Delta(\Omega)$ (EQUATION (39)) IN THE FLYOVER PLANE $\phi = 0$, FOR $\Omega = 0.4, 4, 40$, AND FOR $M = 0.1$, $U_3/U = 0.2$, $2s/L = 0.1$. THE CURVE FOR $\Omega = 4$ HAS BEEN OBTAINED BY USE OF INTERPOLATION CURVES OF THE TYPE SHOWN IN FIGS. 3 – 5.

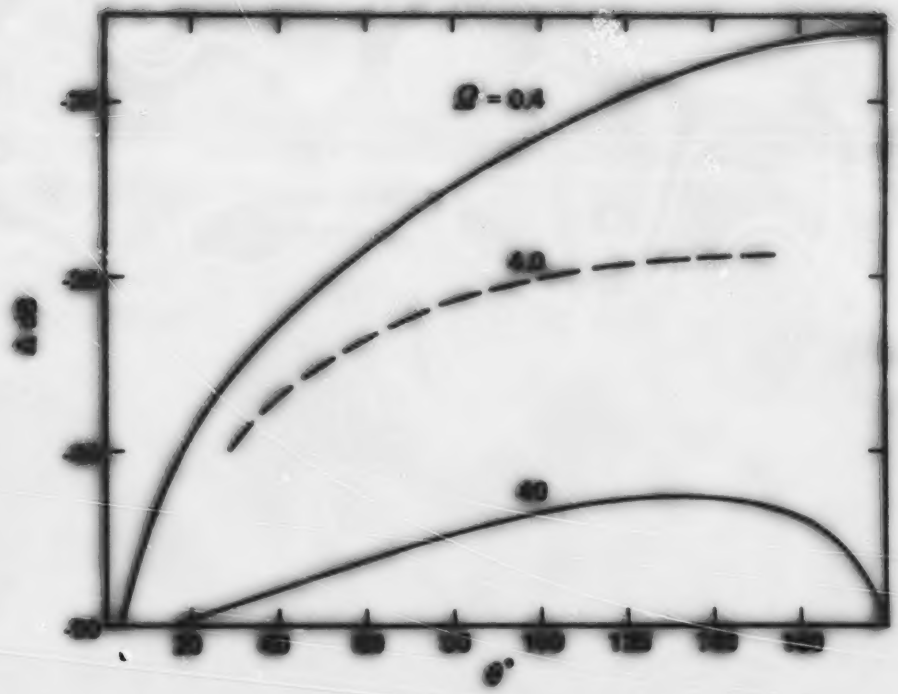

FIG. 7. AS FOR FIG. 6 WITH M = 0.3.

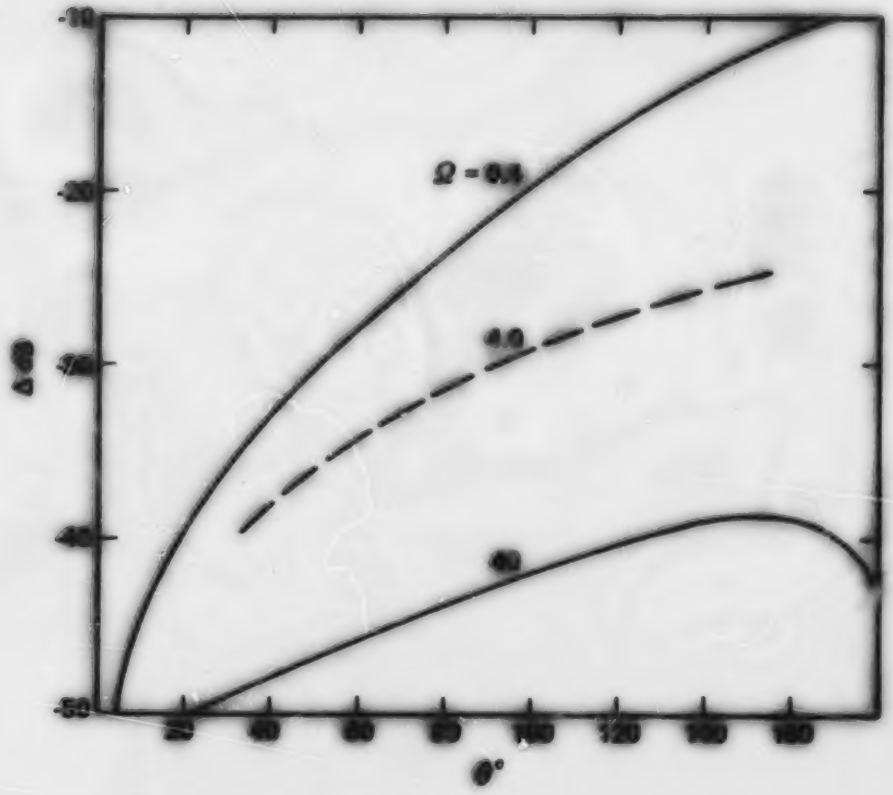

FIG. 8. AS FOR FIG. 6 WITH M = 0.5.

6. COMPARISON WITH EXPERIMENT

The practical application of the formulae derived above requires a knowledge of the effective surface pressure spectrum $\Phi(\omega)$. Measured values of $\Phi(\omega)$ are not yet available, although some of its important characteristics can be inferred from the very recent experiments of Miller [20] in the 40 × 80 ft^2 wind tunnel at the NASA Ames Research Center. These involved a 1/5-full scale model airfoil of 6.7 meter semi-span with three flaps of span 3.43 meters deployed in tandem. The sound generated at the side edges of the flaps at mean flow velocities up to 79 $msec^{-1}$ was found to exceed that from the midspan region by more than 10 dB, the side edge of the leading flaps being the noisiest. The leading flap was deployed at an angle of 20°, and its geometrical configuration relative to the adjacent portion of the airfoil corresponds rather well with the idealized model of Fig. 1. We shall here assume that the associated values of the surface pressure fluctuations provide a good approximation for estimating the noise generated by the side edges of a single deployed flap.

At low mean flow Mach numbers, it was found that the dominant radiation occurred at sufficiently low frequencies that the chord L(~ 20 cms) of the leading flap could be regarded as acoustically compact – the field shape resembled that of a semi-baffled dipole. Cross-correlation measurements of the pressure on the flap indicated that these frequencies satisfied: flap thickness $\lesssim 2\pi U_c/\omega < \frac{1}{2}L$, where $U_c \sim 0.8\ U$ is the characteristic eddy convection velocity. Side edge turbulent velocity fluctuations were in the range 10 – 25% of the mean speed U, corresponding to root mean square surface pressure fluctuations $\sqrt{\overline{p_{se}^2}}$, say, of order 0.01 – 0.06 of the mean dynamic pressure. At the trailing edge of the flap, the root mean square pressure fluctuation $\sqrt{\overline{p_{te}^2}}$, may be identified with that beneath a turbulent boundary layer on a flat plate, and is roughly 0.006 times the mean dynamic pressure [21]. These order of magnitude results can be used to compare the predicted side edge noise with that generated by turbulent flow over the trailing edge of the flap. According to Equations (78), (80) of [7], the acoustic frequency spectrum $S_{te}(\omega)$ of sound generated by trailing edge turbulence is given at low Mach numbers, and in the flyover plane (ϕ=0), by

$$S_{te}(\omega) = \frac{2M_c L_E \ell_3}{\pi r_0^2} \cdot \sin^2(\tfrac{1}{2}\theta)\Phi(\omega) \quad , \tag{44}$$

where L_E is the span of the trailing edge wetted by the turbulent flow, ℓ_3 is the spanwise surface pressure correlation length and, as before $\Phi(\omega)$ denotes the surface pressure frequency spectrum. This result may be combined with the *compact* approximation formula (36) for the side edge noise in order to estimate the relative importance of the two noise producing mechanisms. To do this, we consider a characteristic midrange frequency ω for which $2\pi U_c/\omega \simeq \frac{1}{4}L$. At small mean flow Mach numbers the side edge generated sound pressure level is predicted to exceed that from the trailing edge by an amount ΔSPL, where

$$\Delta SPL = 10 \log_{10}\left|\pi^2 (L/L_E)(\ell_1/\ell_3)\left|H^{(1)}[8\pi(s/L)(U_c/U_3)]\right|^2 I(2s/L)[\overline{p_{se}^2}/\overline{p_{te}^2}]\right| \tag{45}$$

For a flap of chord L = 20 cms deployed at an angle of 20°, the mean value of $2s/L \simeq 0.17$. Interpolation from Table 1 yields $I(2s/L) \simeq 0.053$. Taking $U_c/U = 0.8$, $U_3/U = 0.3$, then gives

$$\left|H_0^{(1)}[8\pi(s/L)(U_c/U_3)]\right|^2 \simeq 0.112 \ .$$

Finally, we take $\ell_1/\ell_3 = 6.5$. This value is appropriate for turbulent boundary layer flow over a flat plate, but it is probably of the correct order in the present case (c.f. [11]). Substituting into Eq. (45), we obtain:

$$\Delta SPL \simeq 10 \log_{10}\{0.38(L/L_E)(\overline{p_{se}^2}/\overline{p_{te}^2})\} \ . \tag{46}$$

Setting L = 20 cms, L_E = 343 cms, we deduce that ΔSPL lies in the range -12 dB to 3.5 dB, when $\overline{p_{se}^2}/\overline{p_{te}^2}$ varies between 2.8, 100 in accordance with the experimental values quoted above. Thus, the noise generated at a single side edge of a part span flap can exceed that generated along the

whole of the trailing edge of the flap by more than 3 dB. The dimensionless form of Eqs. (45) and (46) indicates that this figure extrapolates to full scale without change.

An alternative expression of this conclusion is obtained by taking $L = L_E$ in Eq. (46). This gives a comparison of the effective acoustic source strengths per unit length of side edge/trailing edge. In this case ΔSPL lies between 0.2 – 16 dB, which is entirely consistent with the relative magnitude of 10 dB or more observed by Miller [*20*].

7. CONCLUSIONS

High and low frequency asymptotic formulae have been derived which express the acoustic frequency spectrum in terms of the wavenumber-frequency spectrum of surface pressure fluctuations on the upper surface of a part span flap just in-board of the side edge. From a consideration of approximate versions of these relations it has been concluded that:

1. The radiation has the characteristics of a semi-baffled dipole at small values of the Strouhal number $\omega L/U$ based on the chord of the flap and the forward flight speed. At high frequencies the radiation pattern resembles that of a monopole source.

2. The degree of Doppler amplification due to forward flight of the aircraft is dependent on the Strouhal number $\omega L/U$, being characterized respectively by 3, 2 powers of the Doppler factor $1/(1+M\cos\theta)$ as $\omega L/U \to 0,\infty$. As in the analogous case of noise generated at a trailing edge, there exists a weak dependence on M of the radiation at 90° to the flight path.

3. The radiation efficiency of side edge noise sources is governed by the value of the mean side edge gap Strouhal number $\omega s/U_\infty$ being larger when $\omega s/U_\infty$ is small.

4. Predictions at intermediate Strouhal numbers can be made by interpolation between the low and high frequency formulae.

5. Recent experiments of Miller [*20*] indicate that, at least for small values of the flight Mach number, the dominant radiation from the side edge resembles that of a semi-baffled dipole, the chord of the flap being acoustically compact. Theoretical predictions extrapolated to full scale suggest that the noise generated in this case at a *single* side edge can exceed that generated along the whole of the trailing edge of the flap by 3 dB. This figure is consistent with Miller's experimental findings.

APPENDIX A. THE GREEN'S FUNCTION FOR A NONCOMPACT SLOT

It is required to solve the reciprocal, time-harmonic Eq. (7) for $k_0 L \gg 1$. The width 2s of the slot is assumed to be small compared with the acoustic wavelength. It is sufficient to confine attention to the case in which the reciprocal source at $\underline{x}$ is in the acoustic far field of the slot ($|\underline{x}| \gg L$), and the field point $\underline{y}$ is in the immediate vicinity of the slot. The resulting form of $G(\underline{x},\underline{y})$ is appropriate for use in Eq. (11), in which the aeroacoustic sources are at points $\underline{y}$ near the slot and the observer at $\underline{x}$ is in the far field.

The definitions

$$\left.\begin{aligned}(X_1,Y_1) &= (x_1,y_1)/(1-M^2)^{\frac{1}{2}} \\ K_0 &= k_0/(1-M^2)^{\frac{1}{2}}\end{aligned}\right\} , \tag{A1}$$

$$G = -G(1-M^2)^{\frac{1}{2}} e^{-iK_0 M(X_1-Y_1)} , \tag{A2}$$

enable Eq. (7) to be reduced to:

$$\left(\frac{\partial^2}{\partial Y_1^2} + \frac{\partial^2}{\partial y_2^2} + \frac{\partial^2}{\partial y_3^2} + K_0^2\right) G = \delta(X_1-Y_1)\delta(x_2-y_2)\delta(x_3-y_3) . \tag{A3}$$

When the slot is noncompact, such that much of its length is many acoustic wavelengths from either end, the influence of diffraction at the ends can be neglected in calculating the behavior of G near the slot. The problem accordingly becomes locally two-dimensional, and this feature is exploited by introducing the Fourier transform $\bar{\phi}$ of G:

$$G = \frac{1}{2\pi} \int_{-\infty}^{\infty} \bar{\phi}(y_2,y_3,k) e^{ik(X_1-Y_1)} dk . \tag{A4}$$

Equation (A3) becomes:

$$\left(\frac{\partial^2}{\partial y_2^2} + \frac{\partial^2}{\partial y_3^2} + \gamma^2\right)\bar{\phi} = \delta(x_2-y_2)\delta(x_3-y_3) \ , \tag{A5}$$

where

$$\gamma = (K_0^2-k^2)^{\frac{1}{2}} \tag{A6}$$

and branch-cuts are taken such that on the real k-axis $\mathrm{Im}(\gamma) > 0$ when $|k| > |K_0|$.

The particular solution $\bar{\phi}_1$ of (A5) due to the reciprocal source on the right hand side is

$$\bar{\phi}_1 = -\frac{i}{4} \cdot H_0^{(1)}(\gamma|\bar{y}-\bar{x}|) \ , \tag{A7}$$

where $\bar{y} = (y_2,y_3)$, $\bar{x} = (x_2,x_3)$. Assume for definiteness that $x_2 > 0$. When the cylindrical wave $\bar{\phi}_1$ is incident on the slot, and when end-effects are neglected, the diffracted component $\bar{\phi}_r$ of $\bar{\phi}$ in $y_2 > 0$ may be expressed in the form:

$$\bar{\phi}_r = -\frac{i}{4} \cdot H_0^{(1)}(\gamma|\bar{y}-\bar{x}^s|) + \beta H_0^{(1)}(\gamma|\bar{y}|), \ (|\bar{y}|>>s) \ . \tag{A8}$$

The first term on the right hand side is the specularly reflected field in the absence of the slot due to an image source at $\bar{x}^s = (-x_2,x_3)$. When the wavelength of the incident wave is large compared with the width of the slot, the unsteady flow induced in the slot gives rise to a monopole source of amplitude β which is represented by the second term on the right. In $y_2 < 0$ the influence of diffraction at the trailing edge is important only at points close to the edge. The principal component of the field just below the slot is therefore given by

$$\bar{\phi} = -\beta H_0^{(1)}(\gamma|\bar{y}|) \ , \ (|\bar{y}|>>s) \ , \tag{A9}$$

a monopole equal and opposite in strength to that in Eq. (A8).

At distances from the slot which are very much smaller than the acoustic wavelength, ϕ can be represented by the potential of an essentially incompressible fluid, and we can set

$$\bar{\phi} = A + B\cdot\mathrm{Re}\left\{\ln\left(\frac{z}{s} + \sqrt{\frac{z^2}{s^2} - 1}\right)\right\} , \qquad (A10)$$

where A, B are constants, and $z = y_1 + iy_2$ ([18], §66). The values of s, A, B are determined by matching (A10) with $\phi = \phi_i + \phi_r$ given by (A7,8) and with $\bar{\phi}$ given by (A9) in their respective joint domains of validity.

When the reciprocal source at $\bar{x}$ is in the far field ($\gamma|\bar{x}| >> 1$), and $\bar{y}$ is well within a wavelength of the slot, we can use the following asymptotic expressions for $\bar{\phi}$ given by (A7,8) and (A9)

$$\bar{\phi} = 2Z + s\{1+(2i/\pi)\ln(C\gamma|\bar{y}|/2)\} \quad (y_2 > 0) , \qquad (A11)$$

$$\bar{\phi} = \quad - s\{1+(2i/\pi)\ln(C\gamma|\bar{y}|/2)\} \quad (y_2 < 0) , \qquad (A12)$$

where use has been made of the small argument expansion of the Hankel function $H_0^{(1)}$([17], p. 951), $C = 1.78107...$ is the Euler-Mascheroni constant, and

$$Z = -\tfrac{1}{2}(2i/\pi\gamma|\bar{x}|)^{\frac{1}{2}}e^{i\gamma|\bar{x}|} , \qquad (A13)$$

is the asymptotic form of the incident wave $\bar{\phi}_i$ as $|\bar{y}| \to \infty$. Equations (A11), (A12) are formally valid for

$$2s << |\bar{y}| << 1/|\gamma| .$$

Note that, although $|\gamma|$ can assume *all* positive values, it is only the interval $0<|\gamma|<|k_0|$ which is relevant, wherein the incident disturbance ϕ_i constitutes a propagating wave (γ real).

Similarly, for $|\bar{y}| \doteq |z| >> s$, the local representation (A10) becomes:

$$\bar{\Phi} \simeq A + B\,\mathrm{sgn}(y_2)\cdot\ln(2|\bar{y}|/s) \quad . \tag{A14}$$

Matching this with expressions (A11), (A12) we obtain:

$$A = Z$$

$$B = \frac{2i\beta}{\pi} = \frac{-2iZ}{1+(2i/\pi)\ln(\underline{C}\gamma s/4)} \quad . \tag{A15}$$

The substitution of these results into Eq. (A10), and use of (A4) leads to the approximate representation of $G(\underline{x},\underline{y})$ for points $\underline{y}$ well within an acoustic wavelength of the slot. The integration with respect to k may be evaluated by the method of stationary phase when $|\underline{x}| \to \infty$, yielding

$$G(\underline{x},\underline{y}) \simeq \frac{1}{4\pi R(1-M^2)^{\frac{1}{2}}}\left(1 - \frac{2i\mathrm{Re}\left\{\ln\left(\frac{z}{s}+\sqrt{\frac{z^2}{s^2}-1}\right)\right\}}{\pi[1+(2i/\pi)\ln(\underline{C}K_0 s|\bar{\underline{x}}|/4R)]}\right)$$

$$\times \exp\{iK_0[R+M(Y_1-X_1)]\} \quad , \tag{A16}$$

in which

$$R = \{(X_1-Y_1)^2 + x_2^2 + x_3^2\}^{\frac{1}{2}} \quad . \tag{A17}$$

In the aeroacoustic problem an observer fixed at $\underline{x}$ would be stationary with respect to the airfoil, and would therefore be translating at velocity $(-U,0,0)$ relative to the mean flow. The practical, flyover, case corresponds to an observer at rest relative to the ambient medium, with the aircraft in motion at speed U in the negative x_1-direction. It is then convenient to express the radiation in terms of emission time coordinates (r,θ,ϕ), say, which give the observer position relative to the source at the time at which the received sound was generated. The polar angle θ is measured from the positive direction of the x_1-axis, and

$$\left.\begin{aligned} x_1 - y_1 &= r(M+\cos\theta) \\ x_2 &= r\cos\phi\sin\theta \\ x_3 &= r\sin\phi\sin\theta \end{aligned}\right\} \qquad (A18)$$

It follows that

$$\left.\begin{aligned} R = r(1+M\cos\theta)/(1-M^2)^{\frac{1}{2}};\ R - M(X_1-Y_1) &= r(1-M^2)^{\frac{1}{2}}; \\ |\underline{x}|/R = \sin\theta(1-M^2)^{\frac{1}{2}}/(1+M\cos\theta)\ , & \end{aligned}\right\} \qquad (A19)$$

and therefore that expression (A16) for $G(\underline{x},\underline{y})$ assumes the form:

$$G(\underline{x},\underline{y}) =$$

$$\frac{e^{ik_0 r}}{4\pi r(1+M\cos\theta)}\left\{1 - \frac{2i\mathrm{Re}\left\{\ln\left(\frac{z}{s} + \sqrt{\frac{z^2}{s^2} - 1}\right)\right\}}{\pi\left(1+(2i/\pi)\ln[\underline{C}k_0 s\cdot\sin\theta/4(1+M\cos\theta)]\right)}\right\}. \qquad (A20)$$

APPENDIX B. THE GREEN'S FUNCTION FOR A COMPACT SLOT

An approximate solution of Eq. (A3) will now be obtained in the compact limit for which

$$k_0 L/(1-M^2) \equiv K_0 L' << 1 ,$$

where

$$L' = L/(1-M^2)^{\frac{1}{2}} . \tag{B1}$$

In this case the length scale of variation of G in the neighborhood of the slot is small compared with $1/K_0$. This implies that K_0^2 on the left of Eq. (A3) can be discarded when the field point (Y_1, y_2, y_3) is close to the slot, where, in a leading approximation, G will satisfy the Laplace equation.

When the slot is absent the incident and diffracted fields G_0 due to the reciprocal source on the right of (A3) can be expanded in terms of Bessel and Hankel functions in the form:

$$G_0 = \frac{-i}{8\pi} \sum_{n=0}^{\infty} \int_{-\infty}^{\infty} \varepsilon_n \cos[\tfrac{1}{2}n(\bar{\theta}_0-\pi)]\cos[\tfrac{1}{2}n(\bar{\theta}-\pi)]J_{n/2}(\gamma\rho_0)H_{n/2}^{(1)}(\gamma\rho)$$

$$\times e^{ik(x_3-y_3)} dk \quad (\rho_0<\rho) , \tag{B2}$$

where γ is given by Eq. (A6),

$$\varepsilon_0 = 1, \ \varepsilon_n = 2 \ (n = 1,2,3,\ldots) ,$$

and $(\rho,\bar{\theta})$, $(\rho_0, \bar{\theta}_0)$ are polar coordinates defined by

$$(X_1,x_2) = \rho(\cos\bar{\theta},\sin\bar{\theta}); \ (Y_1,y_2) = \rho_0(\cos\bar{\theta}_0,\sin\bar{\theta}_0) ,$$

(see, e.g., Bowman *et al.* [19] Chapter 8).

When $K_0(X_1^2+x_2^2+x_3^2)^{\frac{1}{2}} >> 1$, and $K_0(Y_1^2+y_2^2+y_3^2)^{\frac{1}{2}} << 1$, the integral in (B2) can be evaluated by the method of stationary phase, leading to:

$$G_0 \simeq \frac{-1}{4\pi R_0} \sum_{n=0}^{\infty} \epsilon_n J_{n/2}(K_0\rho_0\rho/R_0)\cos[\tfrac{1}{2}n(\bar{\theta}_0-\pi)]\cos[\tfrac{1}{2}n(\bar{\theta}-\pi)]$$

$$\times e^{i(K_0R_0-n\pi/4)} , \qquad (B3)$$

where

$$R_0 = (X_1^2+x_2^2+x_3^2)^{\frac{1}{2}} . \qquad (B4)$$

Let G_S denote the additional diffracted field in the presence of the slot. This will satisfy Laplace's equation in the vicinity of the slot. At distances from the slot which are large compared with its width 2s yet small relative to $1/K_0$ (i.e., relative to the acoustic wavelength), G_S can be represented by the potential of a line source of strength per unit length $\sigma(Y_1)$, say, which occupies the portion $(-L'<Y_1<0)$ of the Y_1-axis on the upper surface ($y_2 = +0$) of the half-plane, together with a similarly located line *sink* of equal strength on the *lower* surface. This can be expressed in terms of the incompressible limit of Macdonald's representation of the Green's function for a rigid half-plane ([*19*], Chapter 8), from which one finds:

$$G_S = \frac{-\mathrm{sgn}(y_2)}{2\pi} \int_{-L'}^{0} \frac{\sigma(\xi)}{R} \left\{ 1 - \frac{4}{\pi} \cdot \tan^{-1}\left(\frac{R}{R_1+(R_1^2-R^2)^{\frac{1}{2}}} \right) \right\} d\xi . \qquad (B5)$$

where

$$\left.\begin{aligned} R &= \{(Y_1-\xi)^2 + y_2^2 + y_3^2\}^{\frac{1}{2}} \\ R_1 &= \{(\rho_0-\xi)^2 + y_3^2\}^{\frac{1}{2}} \end{aligned}\right\} \quad . \tag{B6}$$

The principal branch of $\tan^{-1}(z)$, which vanishes at $z = 0$, is to be taken in (B5).

Equations (B3), (B5) define

$$G = G_0 + G_S \quad , \tag{B7}$$

in those regions whose closest distance from the slot greatly exceeds the slot width 2s, but is much less than the acoustic wavelength. Provided that $2s \ll L$, the behavior of G at the slot can be taken in a form analogous to (A10), namely:

$$G = A + B(Y_1)\cdot \mathrm{Re}\left\{\ln\left[\frac{z}{s} + \sqrt{\frac{z^2}{s^2} - 1}\right]\right\}, \quad (-L'<Y_1<0) \quad , \tag{B8}$$

where $z = y_3 + iy_2$, A is constant, and $B(Y_1)$ varies significantly only over distances which are large compared with s.

The local source strength $B(Y_1)$ is determined in terms of $\sigma(Y_1)$ as follows. For fixed Y_1 in $(-L',0)$, and for $|z| \gg s$:

$$G \simeq A + B(Y_1)\,\mathrm{sgn}(y_2)\ln(2|z|/s) \quad . \tag{B9}$$

This is valid in the region

$$2s \ll |z| \ll L', \quad -L' < Y_1 < 0 \quad .$$

The formal expression (B9) must be equivalent to that given by (B3, B5, B7) as $|z| \to 0$ $(-L'<Y_1<0)$ in (B7). In this limit the integral in (B5) exhibits a logarithmic singularity of the type occuring in (B9), and equating the coefficients of the logarithms we find:

$$\sigma(Y_1)/\pi = B(Y_1) \quad . \tag{B10}$$

Equations which determine the values of A, $B(Y_1)$ are obtained by matching the remaining, finite terms in (B7), (B9). We do this numerically by partitioning the interval $-L' < Y_1 < 0$ occupied by the slot into N equal parts, each of width $h = L'/N$. The midpoint of the nth partition is at $Y_1 = Y_n$, where

$$Y_n = (n-N-\tfrac{1}{2})h \quad . \tag{B11}$$

Within the range $(Y_n-\frac{1}{2}h,\ Y_n+\frac{1}{2}h)$ $B(Y_1)$ is taken to be constant and equal to B_n. A collocation procedure may now be used to obtain N+1 equations for A, $B_n (n = 1,2,\cdots,N)$. Set $Y_1 = Y_n$ in Eqs. (B7), (B9). Take the limit $|\underline{y}| \equiv |z| \to 0$ in (B7) and match the resulting expression with that on the right of (B9). Making use of the identification (B10) we find:

$$A = -\frac{e^{iK_0R_0}}{4\pi R_0} \quad , \tag{B12}$$

$$B_n \ln(2h/s) + \sum_{m=1}^{N} \tfrac{1}{2}B_m \int_{Y_m-\frac{1}{2}h}^{Y_m+\frac{1}{2}h} \frac{d\xi}{|Y_n-\xi|} \left\{ \varepsilon_{nm} - \frac{4}{\pi}\cdot\tan^{-1}\left[\frac{|Y_n-\xi|}{(|\xi|^{\frac{1}{2}}+|Y_n|^{\frac{1}{2}})^2} \right] \right\}$$

$$= -\frac{e^{iK_0R_0}}{2\pi R_0} (2K_0\rho|Y_n|/i\pi R_0)^{\frac{1}{2}} \sin(\tfrac{1}{2}\bar{\theta}) \quad (n = 1,2,\cdots,N), \tag{B13}$$

in which

$$\left.\begin{aligned} \varepsilon_{nm} &= 0 \quad n = m \\ &= 1 \quad n \neq m \end{aligned}\right\} \quad . \tag{B14}$$

The terms on the right of (B12), (B13) correspond to the inner limit ($|\underline{y}| \to 0$) of G_0 which is given by Eq. (B3). Since $K_0\rho_0 << 1$ in the vicinity of the slot, only the first two terms in the expansion of G_0 in terms of $K_0\rho_0$ have been

retained. The component of the integral on the left of (B13) which involves ϵ_{nm} is evaluated analytically, and that involving the inverse tangent is approximated by means of the trapezoidal formula. The system of linear equations for the B_n turns out to be stable provided that the logarithm shown explicitly on the left hand side of (B13) exceeds unity, i.e. for $2h/s \gtrsim 2.7$.

Set

$$\lambda = |Y_1|/L' = |y_1|/L \ , \tag{B15}$$

and introduce the dimensionless function $m(\lambda)$ defined in terms of $B(Y_1)$ by

$$B(Y_1) = - \frac{m(\lambda)}{2\pi R_0} (2K_0 L'\rho/i\pi R_0)^{\frac{1}{2}} \sin(\tfrac{1}{2}\bar{\theta}) e^{iK_0 R_0} . \tag{B16}$$

The corresponding discrete values m_n satisfy Eqs. (B13) with the right hand sides replaced by $(|Y_n|/L')^{\frac{1}{2}} = \{(N-n+\frac{1}{2})/N\}^{\frac{1}{2}}$, $(n=1,2,\cdots,N)$. The local source strength $B(Y_1)$ and its dimensionless version $m(\lambda)$ are dependent on the slot width/length ratio $2s/L$, and the computed variations of $m(\lambda)$ $(0<\lambda<1)$ for $2s/L = 0.02, 0.05, 0.1$ are depicted in Fig. 2.

Substituting from (B12), (B16) into the local representation (B8) of G, using the definition (A2), and expressing the final result in terms of the emission time coordinates (A18), we obtain, finally,

$$G(\underline{x},\underline{y}) \simeq \frac{e^{ik_0 r_0}}{4\pi r_0 (1+M\cos\theta)} \Bigg\{ 1 + 2m(|y_1|/L)\sin(\tfrac{1}{2}\bar{\theta})[2k_0 L(\rho/R_0)/i\pi(1-M^2)]^{\frac{1}{2}} \times \times \mathrm{Re}\left(\ln\left[\frac{z}{s} + \sqrt{\frac{z^2}{s^2} - 1} \right] \right) \Bigg\} \ , \tag{B17}$$

in which

$$\rho/R_0 = \{(M+\cos\theta)^2+(1-M^2)\cos^2\phi\sin^2\theta\}^{\frac{1}{2}}/(1+M\cos\theta) \ , \qquad (B18)$$

and

$$\sin(\tfrac{1}{2}\bar{\theta}) = \mathrm{sgn}(x_2)\left\{\tfrac{1}{2}\left[1-(M+\cos\theta)/\{(M+\cos\theta)^2+(1-M^2)\cos^2\phi\sin^2\theta\}^{\frac{1}{2}}\right]\right\}^{\frac{1}{2}} \ . \qquad (B19)$$

Equation (B17) gives the compact form of the Green's function for points $\underset{\sim}{y}$ in the immediate vicinity of the slot.

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16. Abstract

A theory is proposed for estimating the noise generated at the side edges of part span trailing edge flaps in terms of pressure fluctuations measured just in-board of the side edge of the upper surface of the flap. Asymptotic formulae are developed in the opposite extremes of Lorentz contracted acoustic wavelength large/small compared with the chord of the flap. Interpolation between these limiting results enables the field shape and its dependence on subsonic forward flight speed to be predicted over the whole frequency range. It is shown that the mean width of the side edge gap between the flap and the undeflected portion of the airfoil has a significant influence on the intensity of the radiated sound. It is estimated that the noise generated at a single side edge of a full scale part span flap can exceed that produced along the whole of the trailing edge of the flap by 3 dB or more.

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